

Digital Holography

Wm. Randall Babbitt
Professor of Physics and Director of Spectrum Lab
Montana State University

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Outline of Tutorial

- Coherent Lidar
- Digital Holography
 - Holography
 - Interference
 - Image Plane DH
 - Pupil plane DH
 - Optical wave propagation
 - Image Recovery – Post-Focusing
 - DH Requirements
 - Signal to Noise
 - Depth of Field

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Digital Holography

The reference wavefront at the film ($z = 0$) is assumed to be a plane wave)

$$E_{ref}(x, y, t) = E_{ref} \cos(2\pi f t - \vec{k}_r \cdot \vec{r} + \phi_{ref}) = \text{real} \left(E_{ref} \exp(i2\pi f t - i\vec{k}_r \cdot \vec{r}) \right)$$

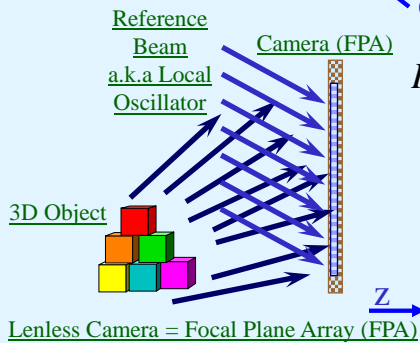
The object wavefront at the film

$$E_{obj}(x, y, t) = A(x, y) \cos(2\pi f t + \phi(x, y)) \\ = \text{real} \left(E_{obj}(x, y) \exp(i(2\pi f t)) \right)$$

$$\text{Note: } \vec{k}_{ref} = k_z \hat{z} + \vec{k}_r \quad |\vec{k}_{ref}| = \frac{2\pi}{\lambda}$$

$$\vec{r} = x\hat{x} + y\hat{y}$$

Assume all light has same polarization



Complex field representation

$$I(x, y) \propto \left\langle \left| E_{obj}(x, y, t) + E_{ref}(x, y, t) \right|^2 \right\rangle_{dt}$$

$$\propto E_{obj}(x, y) E_{ref}^* e^{i\vec{k}_r \cdot \vec{r}} + \text{c.c.}$$

$$+ I_{obj}(x, y) + I_{ref}(x, y)$$

Complex phase and amplitude information is stored in a real-valued spatial interference pattern.

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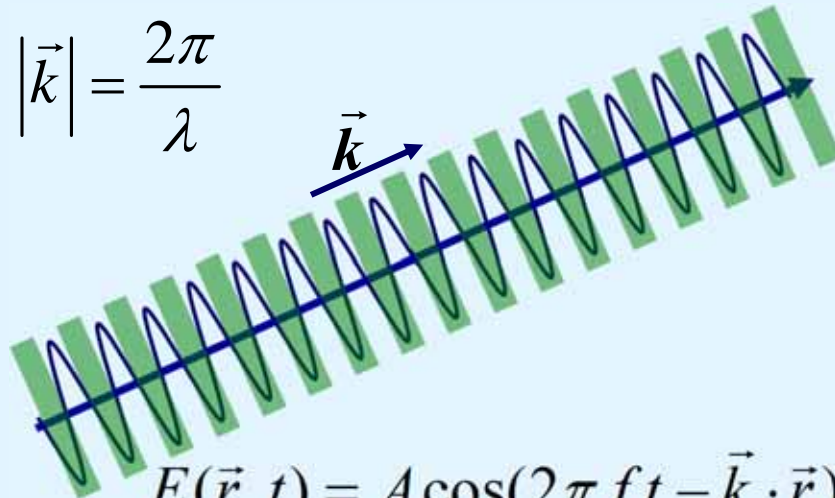
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Wavevectors

Plane wave can travel in any direction

$$|\vec{k}| = \frac{2\pi}{\lambda}$$



$$E(\vec{r}, t) = A \cos(2\pi f t - \vec{k} \cdot \vec{r})$$

The wave vector has a "length" with units 1/meter and wave vector's direction points in direction of wave propagation.

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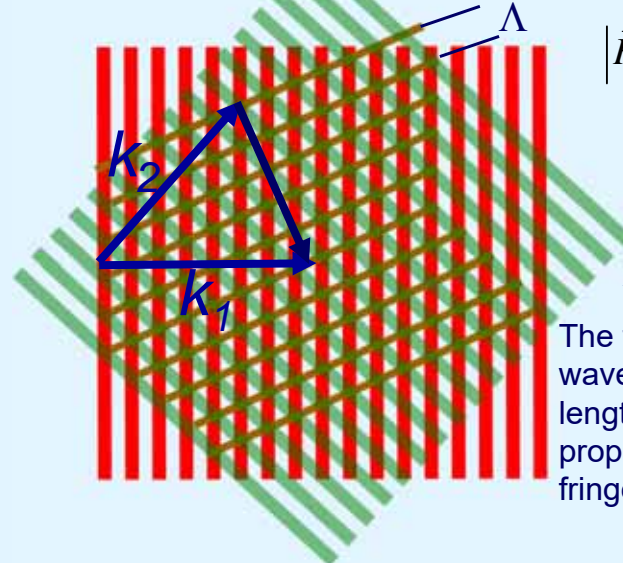
Wave Interference and Wavevectors

Greater angle of interference
 => Longer fringe wavevector
 => Shorter wavelength of fringes

$$|\vec{k}_1| = |\vec{k}_2| = \frac{2\pi}{\lambda}$$

$$\vec{K} = \vec{k}_1 - \vec{k}_2$$

$$|\vec{K}| = 2\pi / \Lambda$$



$$\Lambda = 2\pi / |\vec{K}|$$

The fringe wavevector's length is inversely proportional to the fringe wavelength.

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Pupil Plane vs Image Plane Recording

Pupil plane:

- Object field at camera is FT of field at object
- (+) Wide FOV, no optical elements to cause aberrations
- (-) Small solid angle of light reaches camera
 → low signal strength

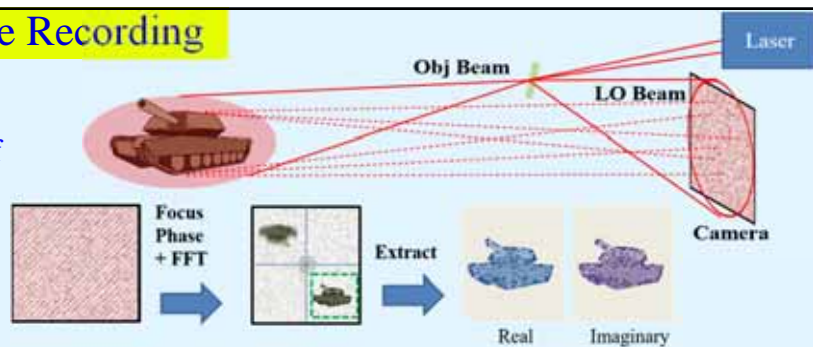
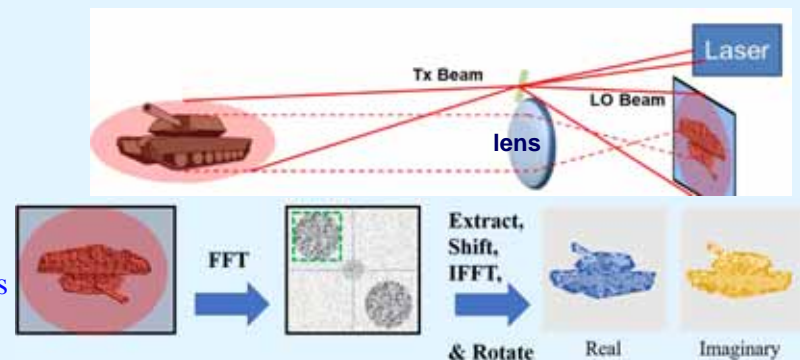


Image plane:

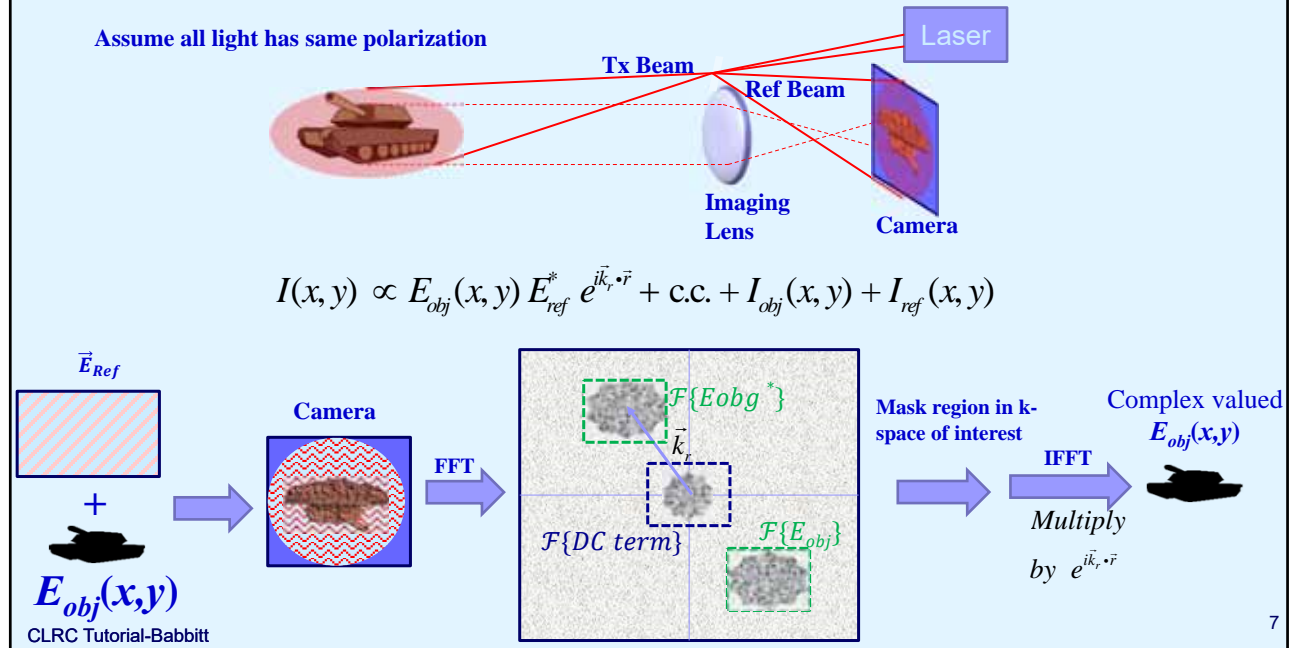
- Object field at camera is scaled copy of field at object
- (+) More light captured
- (-) Aberrations from imaging lens



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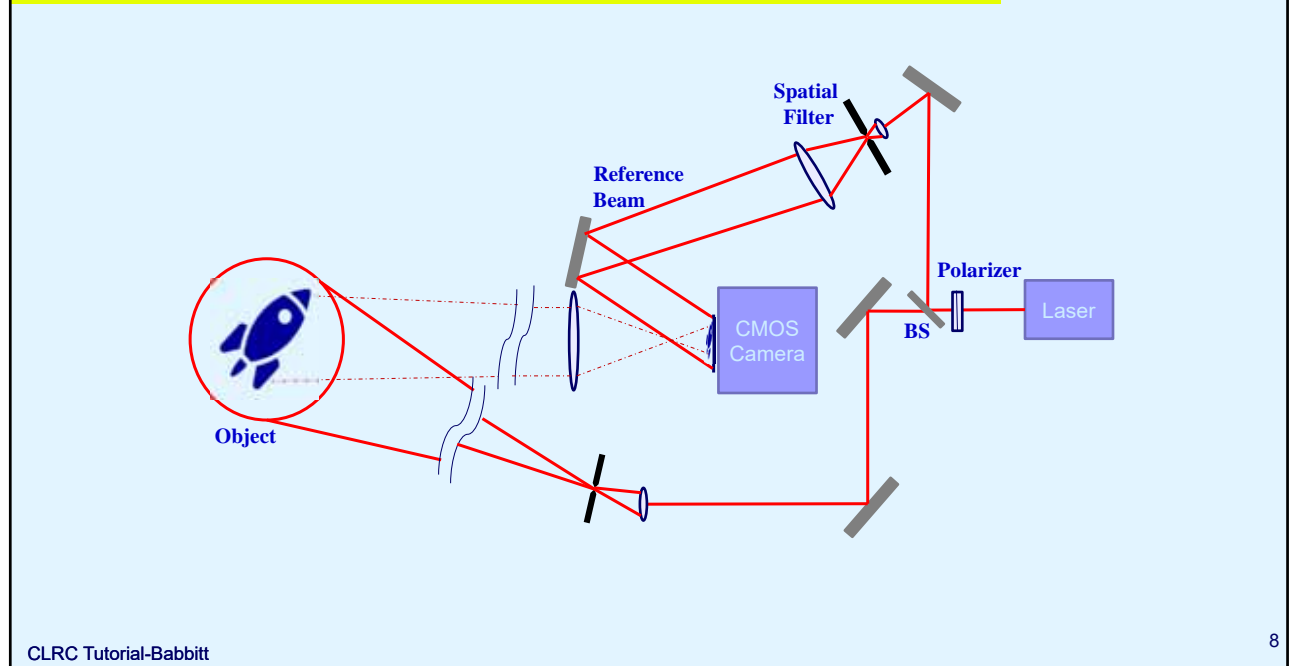
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Digital Hologram Processing: Image Plane Recording



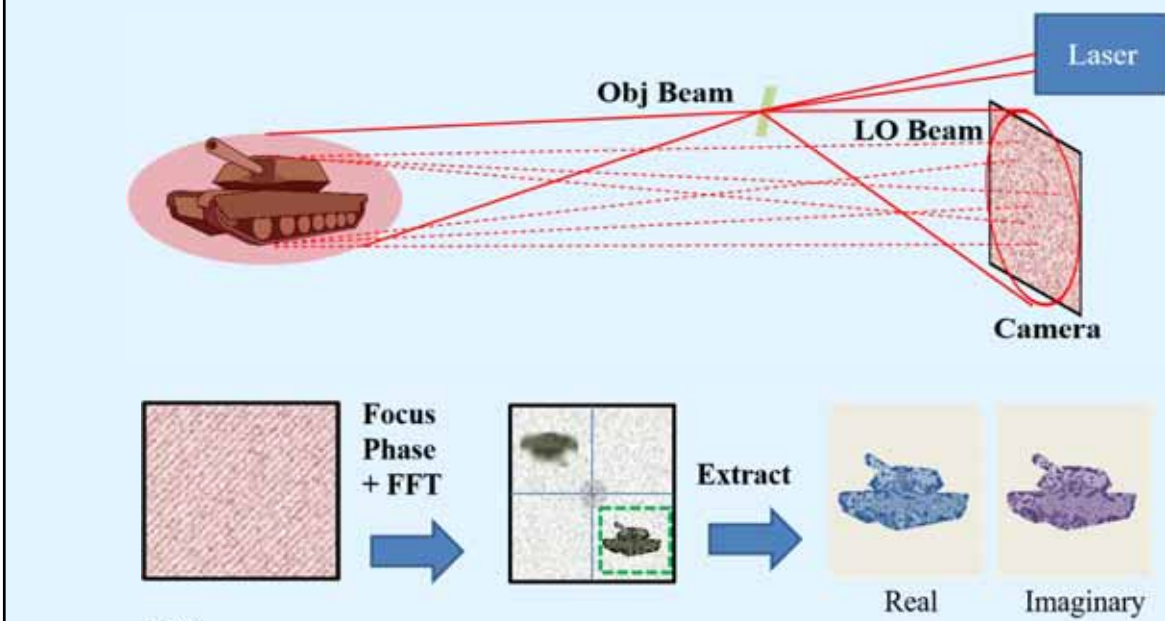
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Digital Holographic Set-up: Image Plane Recording



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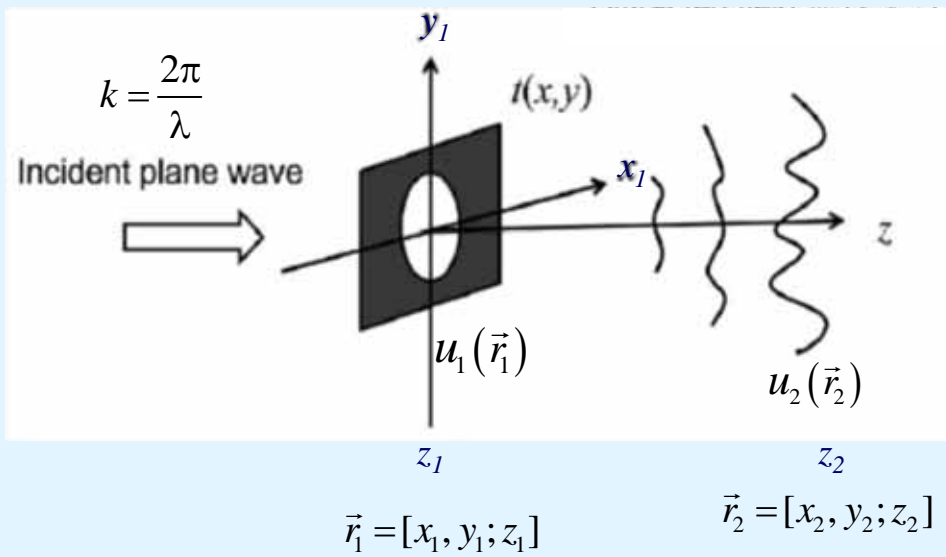
Lenless Holography: Image Plane Recording



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Optical Field Propagation



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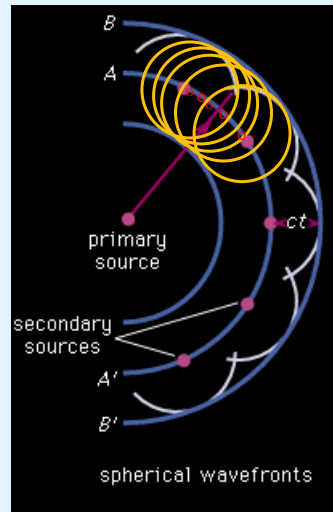
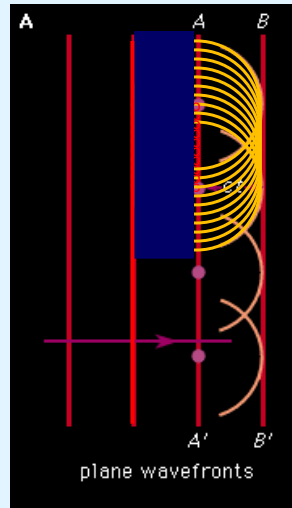
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Wave Propagation Based on Huygens' Principle

Every point on wavefront radiates out a new spherical wave

Radius of each wavefront is ct



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Encyclopedia Britannica

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The Huygens-Fresnel Principle

The *Huygens-Fresnel principle* describes the propagation of optical fields.

Given the optical field at any plane, the field at any other plane is a superposition of spherical waves, known as *Huygens wavelets*, emanating from each point in the first plane, with the phase and amplitude of the field at that point.

$$u_2(\vec{r}_2) = \frac{1}{i\lambda} \iint d^2\vec{r}_1 u_1(\vec{r}_1) \frac{e^{ikR}}{R} \cos\theta$$

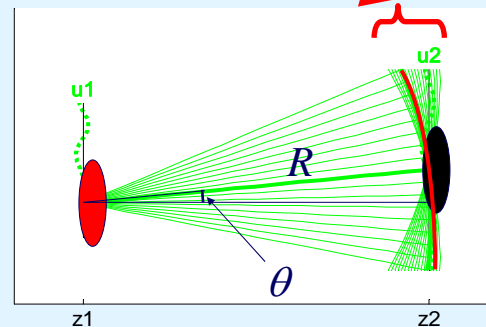
where

$$\vec{r}_1 = [x_1, y_1; z_1], \quad \vec{r}_2 = [x_2, y_2; z_2]$$

$$k = \frac{2\pi}{\lambda}$$

$$R = \sqrt{|\vec{r}_2 - \vec{r}_1|^2 + \Delta z^2}$$

$$\Delta z = z_2 - z_1$$



Note: $\cos(\theta)$ is an inclination factor, which is a bit complicated to explain, but it will be set to one in next slide as part of Fresnel Approximation.

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The Fresnel Approximations

When the transverse (off-axis) distances in the two planes are small compared to the propagation distance Δz , small angle approximations yield useful simplifications: Fresnel Diffraction.

$$u_2(\vec{r}_2) = \frac{1}{i\lambda} \iint d\vec{r}_1 u_1(\vec{r}_1) \frac{e^{ikR}}{R} \cos\theta$$

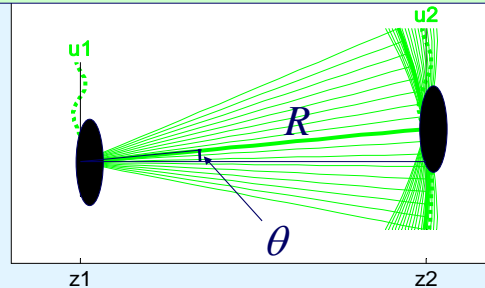
If we assume $|\vec{r}_2 - \vec{r}_1| \ll |\Delta z|$,

$$R = \sqrt{|\vec{r}_2 - \vec{r}_1|^2 + \Delta z^2} \cong \Delta z + \frac{1}{2\Delta z} |\vec{r}_2 - \vec{r}_1|^2$$

$$\frac{1}{R} \cong \frac{1}{\Delta z}$$

$$e^{ikR} \cong e^{ik\Delta z} \cdot \exp\left(\frac{ik}{2\Delta z} |\vec{r}_2 - \vec{r}_1|^2\right)$$

$$\cos\theta \cong 1$$



The Fresnel diffraction integral:

$$u_2(\vec{r}_2) \cong \frac{e^{ik\Delta z}}{i\lambda\Delta z} \iint d^2\vec{r}_1 u_1(\vec{r}_1) \exp\left(\frac{ik}{2\Delta z} |\vec{r}_2 - \vec{r}_1|^2\right)$$

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Fourier Optics - Fresnel Propagation

$$u_2(\vec{r}_2) \cong \frac{e^{ik\Delta z}}{i\lambda\Delta z} \iint d^2\vec{r}_1 u_1(\vec{r}_1) \exp\left(\frac{ik}{2\Delta z} |\vec{r}_2 - \vec{r}_1|^2\right)$$

In terms of x and y coordinates at z_1 and z_2

$$u_2(x_2, y_2) \cong \frac{e^{ik\Delta z}}{i\lambda\Delta z} \iint dx_1 dy_1 u_1(x_1, y_1) \exp\left(\frac{ik}{2\Delta z} ((x_2 - x_1)^2 + (y_2 - y_1)^2)\right)$$

Assuming initial field and region of interest for the final field are centered close to axis, and propagation in positive z, the Fresnel condition is:

$$|\vec{r}_2 - \vec{r}_1| \ll |\Delta z| \quad \text{for all } \vec{r}_2, \vec{r}_1$$

\Rightarrow

$$|x_1| \ll \Delta z, |y_1| \ll \Delta z, |x_2| \ll \Delta z, |y_2| \ll \Delta z \quad \text{for all } x_1, y_1, x_2, y_2$$

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Fourier Optics - Fresnel Propagation

$$\begin{aligned}
 u_2(x_2, y_2) &\cong \frac{e^{ik\Delta z}}{i\lambda\Delta z} \iint dx_1 dy_1 u_1(x_1, y_1) \exp\left(\frac{ik}{2\Delta z} \left((x_2 - x_1)^2 + (y_2 - y_1)^2\right)\right) \\
 &= \frac{ke^{ik\Delta z}}{i2\pi\Delta z} \exp\left(\frac{ik(x_2^2 + y_2^2)}{2\Delta z}\right) \iint dx_1 dy_1 \left(u_1(x_1, y_1) \exp\left(\frac{ik(x_1^2 + y_1^2)}{2\Delta z}\right) \right) \exp\left(\frac{ik(x_2 x_1 + y_2 y_1)}{\Delta z}\right)
 \end{aligned}$$

quadratic
phase
factors

$$k_x = \frac{kx_2}{\Delta z} \quad k_y = \frac{ky_2}{\Delta z}$$

scaled Fourier transform

$$u_2(x_2, y_2) = \frac{ke^{ik\Delta z}}{i2\pi\Delta z} \exp\left(\frac{ik(x_2^2 + y_2^2)}{2\Delta z}\right) \iint dx_1 dy_1 \left(u_1(x_1, y_1) \exp\left(\frac{ik(x_1^2 + y_1^2)}{2\Delta z}\right) \right) \exp(ik_x x_1 + ik_y y_1)$$

The Fresnel diffraction integral decomposes into a sequence of three operations:

1. Multiply initial field by a quadratic phase factor
2. Do a scaled Fourier transform
3. Multiply by a quadratic phase factor.

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2D Fourier Transform (2D FT)

The 2D Fourier Transform of a continuous, non-periodic function $f(x, y)$ is defined as follows:

$$\mathbf{F}_{2D}(f(x, y)) = F(k_x, k_y) = \frac{1}{2\pi} \int \int_{-\infty}^{\infty} f(x, y) e^{-ik_x x} e^{-ik_y y} dx dy$$

Given $F(k_x, k_y)$, we can obtain $f(x, y)$ back using the 2D Inverse Fourier Transform (2D-IFT):

$$\mathbf{F}_{2D}^{-1}(F(k_x, k_y)) = \frac{1}{2\pi} \int \int_{-\infty}^{\infty} F(k_x, k_y) e^{ik_x x} e^{ik_y y} dk_x dk_y = f(x, y)$$

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Fourier Optics - Fraunhofer Propagation

$$u_2(x_2, y_2) \cong \frac{ke^{ik\Delta z}}{i2\pi\Delta z} \exp\left(\frac{ik(x_2^2 + y_2^2)}{2\Delta z}\right) \iint dx_1 dy_1 \left(u_1(x_1, y_1) \exp\left(\frac{ik(x_1^2 + y_1^2)}{2\Delta z}\right) \right) \exp\left(\frac{ik(x_2 x_1 + y_2 y_1)}{\Delta z}\right)$$

If the initial object is “small” compared $\sqrt{\lambda\Delta z}$

$$\frac{k}{2\Delta z} (x_1^2 + y_1^2) \ll \pi$$

$$\Rightarrow |r_1| = \sqrt{(x_1^2 + y_1^2)} \ll \sqrt{\lambda\Delta z}, \text{ for all } x_1, y_1$$

Then the far field is just the Fourier Transform of the image (with a quadratic phase factor)

$$u_2(x_2, y_2) \cong \frac{ke^{ik\Delta z}}{i2\pi\Delta z} \exp\left(\frac{ik(x_2^2 + y_2^2)}{2\Delta z}\right) \iint dx_1 dy_1 u_1(x_1, y_1) \exp\left(\frac{ik}{\Delta z}(x_2 x_1 + y_2 y_1)\right)$$

Fraunhofer Diffraction Pattern

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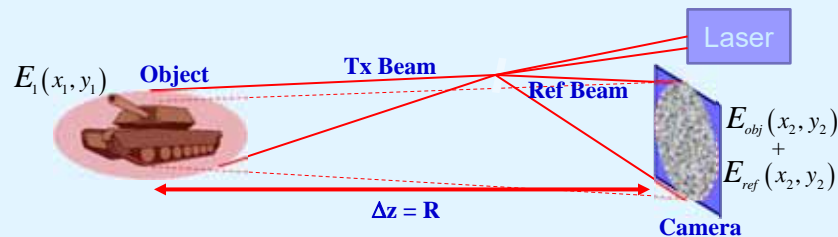
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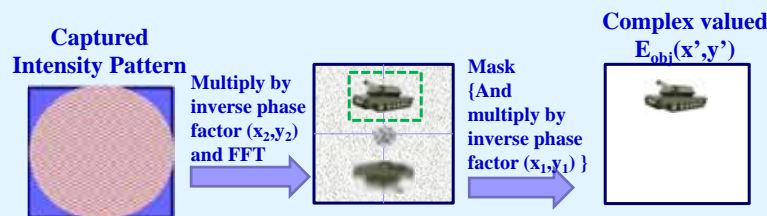
Digital Holography: Pupil Plane Recording (Lenless)

Object field after propagation from Object plane to Camera plane without lens

$$E_{obj}(x_2, y_2) = \frac{ke^{ikR}}{i2\pi R} \exp\left(\frac{ik(x_2^2 + y_2^2)}{2R}\right) \iint dx_1 dy_1 \left(E_1(x_1, y_1) \exp\left(\frac{ik(x_1^2 + y_1^2)}{2R}\right) \right) \exp(ik_x x_1 + ik_y y_1)$$



$$I(x_2, y_2) \propto E_{obj}(x_2, y_2) E_{ref}^* e^{ik_r \cdot \vec{r}_2} + \text{c.c.} + I_{obj}(x_2, y_2) + I_{ref}(x_2, y_2)$$



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Pupil Plane Processing to get Image Intensity

Object field in camera plane without lens

$$E_{obj}(\vec{r}_2) = \frac{ke^{ikR}}{i2\pi R} \exp\left(\frac{ik|\vec{r}_2|^2}{2R}\right) \iint d\vec{r}_1 \left(E_1(\vec{r}_1) \exp\left(\frac{ik|\vec{r}_1|^2}{2R}\right) \right) \exp(i\vec{k}_s \cdot \vec{r}_1)$$

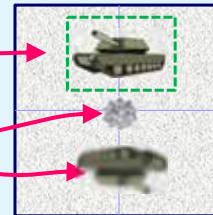
Recorded intensity

$$I(\vec{r}_2) \propto E_{obj}(\vec{r}_2) E_{ref}^* e^{i\vec{k}_r \cdot \vec{r}_2} + \text{c.c.} + I_{obj}(\vec{r}_2) + I_{ref}(\vec{r}_2)$$

$$\vec{k}_s = \frac{kx_2}{R} \hat{x}_1 + \frac{ky_2}{R} \hat{y}_1$$

Pupil Plane Digital Hologram Processing:

1. Capture $I(r_2)$ with DH system
2. Multiply capture field by complex conjugate of quadratic phase factor (yellow boxes)
3. Do a scaled Inverse Fourier transform to get object field



Computed object field (still with quadratic phase factor) in primed image plane

1. $E_1(r_1)$ is object field in object plane
2. $E_1(r_1')$ is object field in primed image plane

$$u_1'(\vec{r}_1') \propto \mathcal{F}_{scaled}^{-1} \left\{ \exp\left(\frac{-ik|\vec{r}_2|^2}{2R}\right) I(\vec{r}_2) \right\} \propto E_1(\vec{r}_1' - \vec{r}_{shift}) \exp\left(\frac{ik|\vec{r}_1' - \vec{r}_{shift}|^2}{2R}\right) + \dots$$

$$|u_{1,masked}'(\vec{r}_1')|^2 \propto I_1(\vec{r}_1' - \vec{r}_{shift})$$

Unshifted or shifted by scaled \vec{k}_r

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Pupil Plane Processing to get Image Amplitude

Object field in camera plane

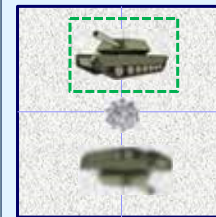
$$E_{obj}(\vec{r}_2) = \frac{ke^{ikR}}{i2\pi R} \exp\left(\frac{ik|\vec{r}_2|^2}{2R}\right) \iint d\vec{r}_1 \left(E_1(\vec{r}_1) \exp\left(\frac{ik|\vec{r}_1|^2}{2R}\right) \right) \exp(i\vec{k}_s \cdot \vec{r}_1)$$

Recorded intensity

$$I(\vec{r}_2) \propto E_{obj}(\vec{r}_2) E_{ref}^* e^{i\vec{k}_r \cdot \vec{r}_2} + \text{c.c.} + I_{obj}(\vec{r}_2) + I_{ref}(\vec{r}_2)$$

Pupil Plane Digital Hologram Processing:

1. Capture $I(r_2)$ with DH system
2. Multiply capture field by c.c. of quadratic phase factor (yellow boxes)
3. Do a scaled Inverse Fourier transform
4. Mask if desired (stop here if you just want object intensity, $|u_1|^2$)
5. Multiply by c.c. of quadratic phase factor (red boxes) to get complex u_1



Computed complex reimaged object field

$$u_1'(\vec{r}_1') \propto \exp\left(\frac{-ik|\vec{r}_1'|^2}{2R}\right) \mathcal{F}_{scaled}^{-1} \left\{ \exp\left(\frac{-ik|\vec{r}_2|^2}{2R}\right) I(\vec{r}_2) \right\} \propto E_1(\vec{r}_1' - \vec{r}_{shift}) + \dots$$

Note the quadratic phase factors are functions of R , which allows

- post-capture focusing of the object(s)
- processing multiple objects by bringing each into focus separately.

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DH – Pupil Plane Recording – Diffraction Limits

If the initial object is “small” compared $\sqrt{\lambda\Delta z}$

$$|\vec{r}_1| = \sqrt{(x_1^2 + y_1^2)} \ll \sqrt{\lambda\Delta z}, \text{ for all } x_1, y_1 \text{ for which object is non-zero}$$

Then you don't need to worry about quadratic phase factor with x_1 and y_1 and only worry about quadratic phase factor with x_2 and y_2 if complex field is desired (Fraunhofer regime)

$$u_2(x_2, y_2) \cong \frac{ke^{ik\Delta z}}{i2\pi\Delta z} \exp\left(\frac{ik(x_2^2 + y_2^2)}{2\Delta z}\right) \iint dx_1 dy_1 (u_1(x_1, y_1)) \exp\left(\frac{ik(x_2x_1 + y_2y_1)}{\Delta z}\right)$$

If the captured image is “small” compared $\sqrt{\lambda\Delta z}$

$$|\vec{r}_2| = \sqrt{(x_2^2 + y_2^2)} \ll \sqrt{\lambda\Delta z}, \text{ for all } x_2, y_2 \text{ for which } u_2(x_2, y_2) \text{ is non-zero}$$

Still need to worry about quadratic phase terms (NOT Fraunhofer regime)

$$u_2(x_2, y_2) \cong \frac{ke^{ik\Delta z}}{i2\pi\Delta z} \iint dx_1 dy_1 \left(u_1(x_1, y_1) \exp\left(\frac{ik(x_1^2 + y_1^2)}{2\Delta z}\right) \right) \exp\left(\frac{ik(x_2x_1 + y_2y_1)}{\Delta z}\right)$$

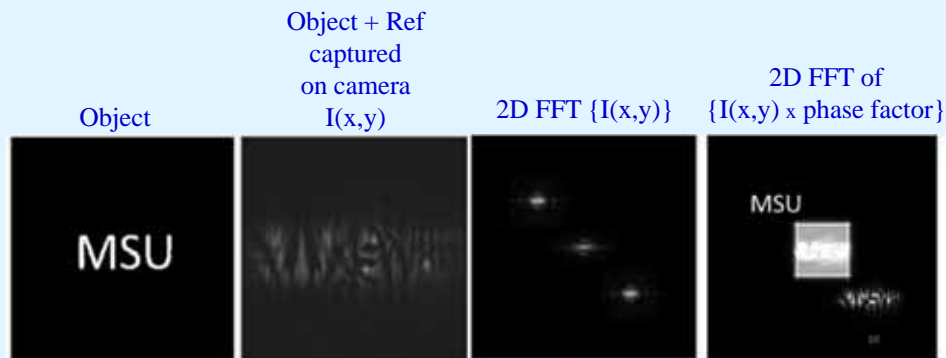
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Pupil Plane Digital Holography: Simulation Example

$$u_1'(\vec{r}_1') \propto \exp\left(\frac{-ik|\vec{r}_1'^2}{2R}\right) \mathbf{F}_{scaled}^{-1} \left\{ \exp\left(\frac{-ik|\vec{r}_2'^2}{2R}\right) I(\vec{r}_2) \right\} \propto E_1(\vec{r}_1' - \vec{r}_{shift}) + \dots$$



Equation above is for general field, used if you want to recover the complex field. In this example, we just wanted object intensity, so outside quadratic phase term is ignored

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Images courtesy of Matt Goodman, MSU Spectrum Lab

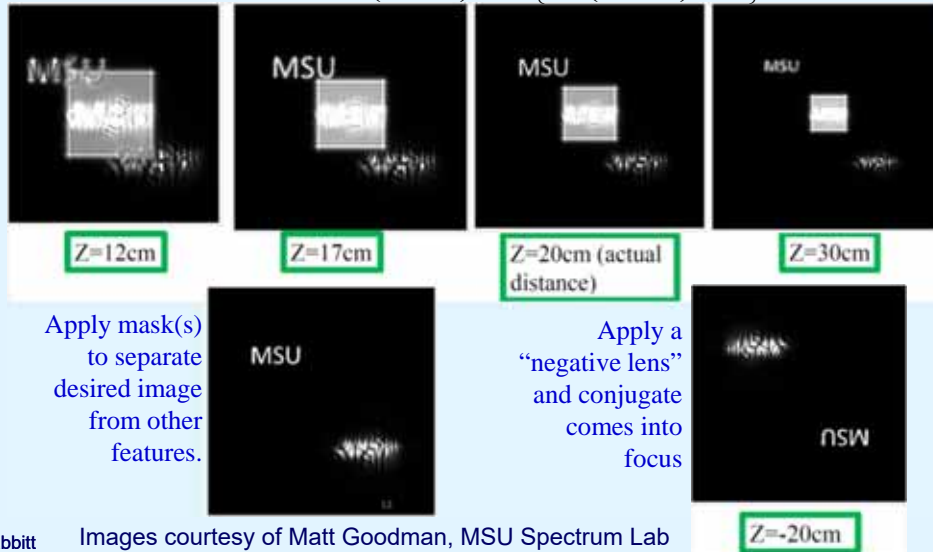
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Pupil Plane Digital Holography: Refocussing

Varying the phase factor (focal distance $Z (=R)$)

$$u_1'(\vec{r}_1') \propto \exp\left(\frac{-ik|\vec{r}_1'|^2}{2R}\right) \mathbf{F}_{scaled}^{-1} \left\{ \exp\left(\frac{-ik|\vec{r}_2'|^2}{2R}\right) I(\vec{r}_2') \right\} \propto E_1(\vec{r}_1' - \vec{r}_{shift}) + \dots$$



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Images courtesy of Matt Goodman, MSU Spectrum Lab

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DH - Requirements

- **Stable laser:**
 - Single Frequency
 - Coherence length greater than object-reference difference
 - Wavelength that matches system requirements
- **Spatial stability**
 - Path difference constant to better than $\lambda/4$ during exposure
 - The faster the exposure, the better.
- **Post-processing**
 - Preferred: Real-time camera capture and post-processing
 - -Fast data link with camera followed by fast CPU, FPGA, or GPU
- **Local Oscillator/Reference Beam**
 - High spatial coherence
 - Preferred: plane wave
 - Spherical wave: just multiply in post-processing by it's quadratic wavefront
 - Angled w.r.t. Object beam (unless implementing phase shifted DH)
- **Camera**
 - Operation at system wavelength
 - Preferred: Fast frame rate
 - Number of pixels: Trade-off between resolution and frame rate
 - Pixel size: Smaller size => higher LO angles, but less object resolution (w/ fixed # of pixels).

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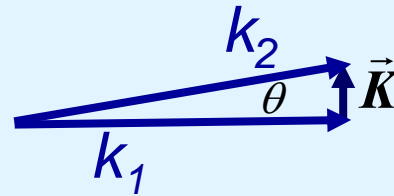
Reference-Object Angle and Camera Pixel Spacing

For small angle of separation, θ , of the object and reference waves

$$\vec{K} = \vec{k}_2 - \vec{k}_1 \sim k\theta = 2\pi\theta / \lambda$$

And the fringe wavelength, Λ , is roughly

$$\Lambda = 2\pi / |\vec{K}| \approx \lambda / \theta$$



To capture the fringes on the camera, it is good to have the spacing of the pixel of the camera, s , to be smaller than $\frac{1}{2} \Lambda$, Nyquist limit

$$s \leq \Lambda / 2 \approx \lambda / (2\theta)$$

Given a fixed pixel size on the camera and fixed operating wavelength, the maximum angle between object and reference is

$$\theta_{max} \approx \lambda / (2s)$$

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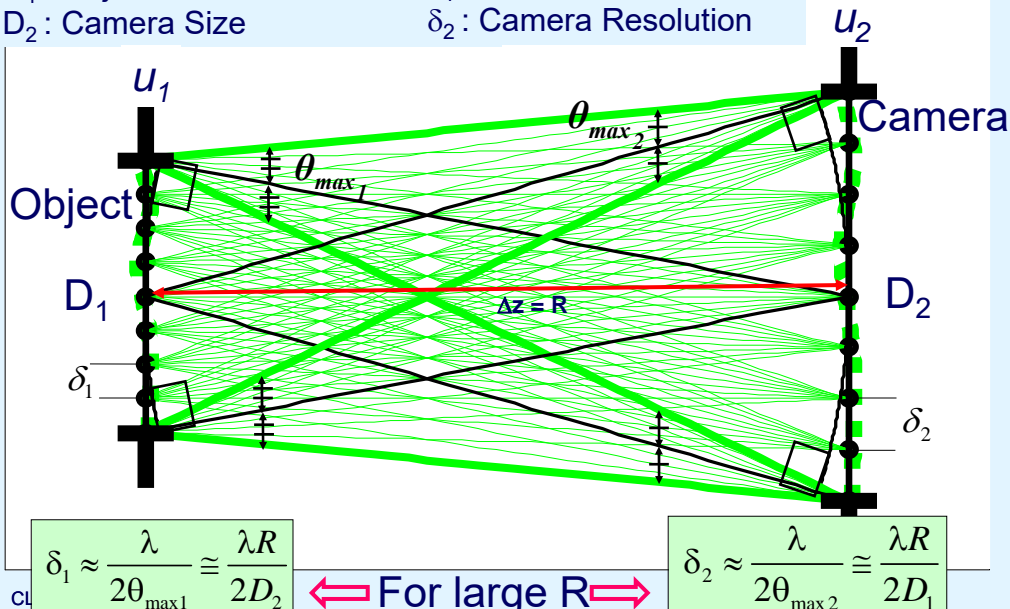
Nyquist Criteria for Sampling Object Field

D_1 : Object Size

δ_1 : Object Resolution

D_2 : Camera Size

δ_2 : Camera Resolution



Resolution requirements in addition to accounting for angled reference beam.

$$\delta_1 \approx \frac{\lambda}{2\theta_{max1}} \cong \frac{\lambda R}{2D_2}$$

For large $R \Rightarrow$

$$\delta_2 \approx \frac{\lambda}{2\theta_{max2}} \cong \frac{\lambda R}{2D_1}$$

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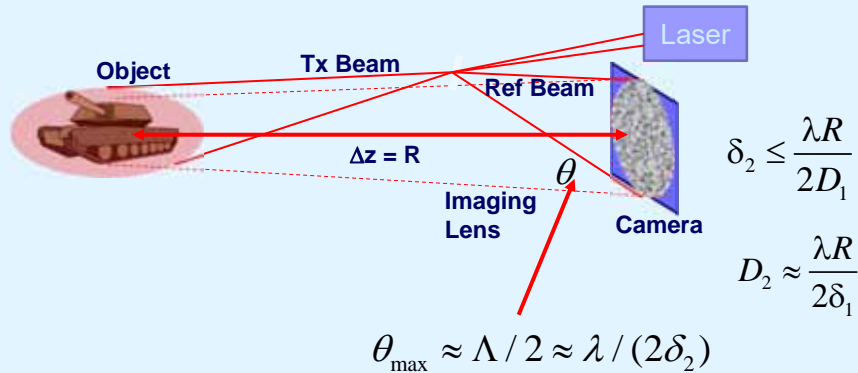
DH: Pupil Plane Recording - Requirements

D_1 : Object Size

δ_1 : Object Resolution

D_2 : Camera Size

δ_2 : Camera Resolution



For image plane recording: Camera resolution and size should “match” object’s image resolution and size, not accounting for angled reference beam.

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DH Signal-to-Noise

- After masking and inverse Fourier transforming, we obtain estimate of complex field for reconstructed image

$$E_{\text{Reconstruct}} \approx E_{LO}^* U \propto \sqrt{\bar{m}_{LO}} \bar{m}_s$$

$$SNR = \frac{\sqrt{\bar{m}_{LO}} \sqrt{\bar{m}_s}}{\sqrt{\bar{m}_{LO}} + \sqrt{\bar{m}_s} + \sigma_N}$$

- If $\bar{m}_{LO} \gg \bar{m}_s$

$$SNR = \frac{\sqrt{\bar{m}_{LO}} \sqrt{\bar{m}_s}}{\sqrt{\bar{m}_{LO}} + \sigma_N}$$

Typically set LO power to produce $\bar{m}_{LO} < \approx$ well depth

- If the number of photoelectrons generated from LO field is much greater than camera readout noise, $\sqrt{\bar{m}_{LO}} > \sigma_N$

$$SNR \approx \sqrt{\bar{m}_s}$$

- The system SNR is then limited by the shot noise of the signal

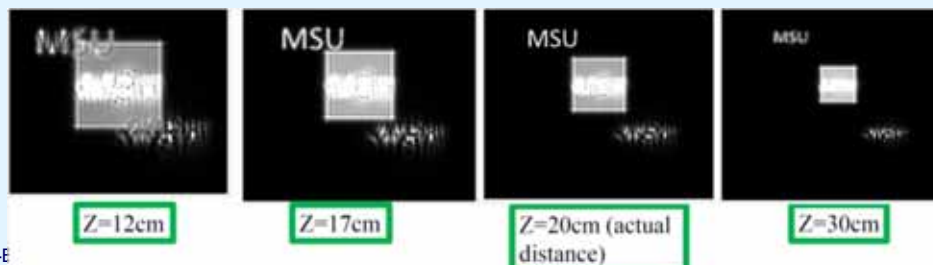
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Depth of Field (DOF)

- For conventional imaging and CW DH, the Depth of Field (DOF) is axial distance around “focused” object plane over which the image is in “focus”.

- Diffraction Limited: $DOF_{DL} = 2\lambda \left(\frac{R}{D}\right)^2$, R : Object Range
 D : Entrance pupil diameter
- Feature Limited: $DOF_{NDL} = 2\delta \frac{R}{D}$. δ : Feature size



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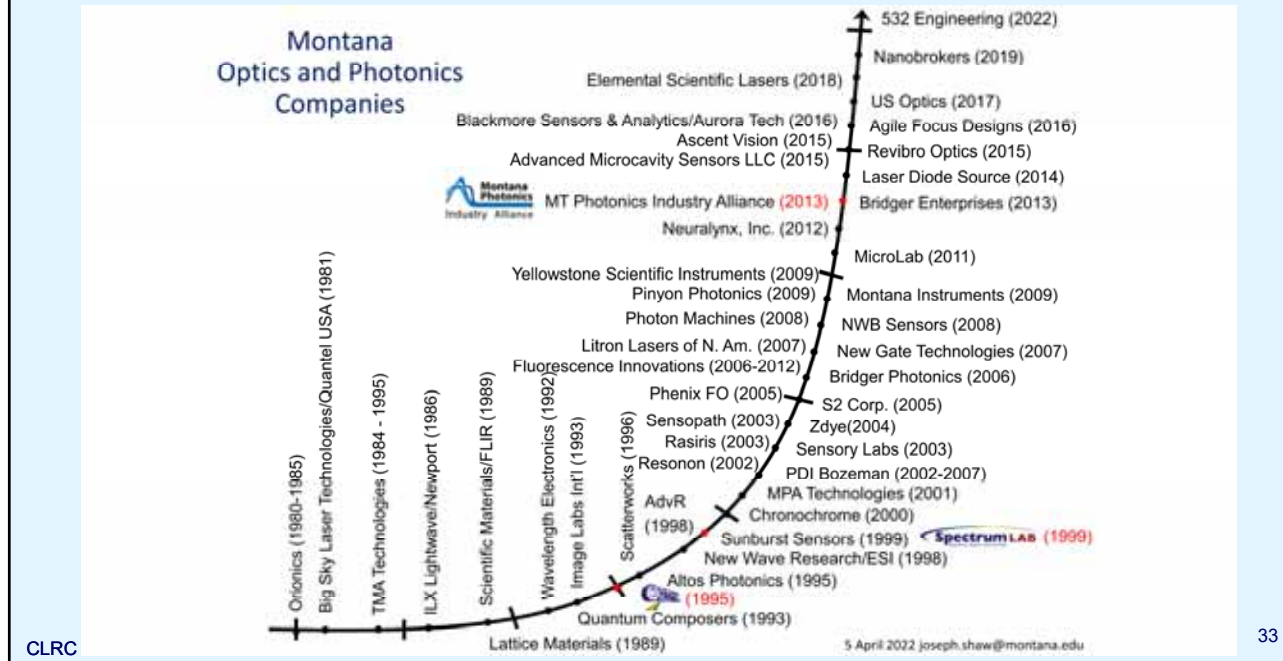
Montana Photonics Industry Alliance (MPIA)

- MSU helped found the MPIA
- MSU faculty and staff serve on the MPIA Board of Directors
- MSU and MPIA collaborate continuously to grow and sustain relationships in Montana and world-wide

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Montana Optics and Photonics Companies



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Spectrum Lab Overview

History

- Montana State University Research Center since 1999
- Research Expenditures/Assets
 - >\$1M per year in research expenditures
 - >>\$2M of accumulated equipment for optics and photonics research
- Research Spin-offs
 - Four successful (25-75 employees, >>\$1M annual revenue) direct and indirect "research spin off" companies
 - S2 Corporation, Bridger Photonics, Blackmore Sensors/Aurora, Montana Instruments

Spectrum Lab's Mission

- Develop and help commercialize Montana grown photonic technologies.
- Transfer developed technologies to Montana companies.
- Provide enhanced educational and employment opportunities for Montana undergraduate and graduate students.

Expertise

- Applied Research and Development: Spatial-Spectral Holography, Microwave photonics, Precision Lidar, Coherent Imaging, Laser Development
- Interdisciplinary Research: Students/Collaborators in Optics and Photonics, Physics, Material Science, Electrical and Computer Engineering, and Mechanical Engineering
- IP generation and protection => Fostering research spin-offs
- Educating students for careers in optics and photonics industry.
- Controlled unclassified (CUI) research facility. Personnel at secret and higher.

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Recent Spectrum Lab Projects



- **Coherent Lidar and Imaging**
 - Stable, Linearized Optical Chirps
 - Range-Resolved Digital Holographic Imaging (See Thursday talk by Matt Goodman)
 - Polarimetric Digital Holography
 - Imaging through Turbulence and Fog (See Thursday talk by Corey Pearson)
 - Temporal Heterodyne Range-Resolved Digital Holography (See Monday Poster by Cole Hammond)

- **Quantum Networks**
 - Quantum information transfer in free space and through multi-core fibers
 - Materials for quantum memories and sources

- **Spatial-Spectral Holographic Microwave Signal Processors**
 - Microwave Photonics
 - » Extremely broadband, high resolution spectrum monitoring and geolocation
 - 0-110 GHz, 40 GHz IBW, sub-MHz resolution, >1 KHz frame rates, >60 dB SFDR
 - » Broadband, high SFDR analog photonics links
 - Real-Time High Bandwidth Correlator
 - » Broadband “noise” radar and geolocation
 - » Massively parallel cyclostationary signal processing